

# Frequency-Agile LIDAR Receiver for Chemical and Biological Agent Sensing

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**Report Documentation Page** 

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### **Overview**



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- Objective: Improve standoff range and chem-bio agent detection limits of direct detection LWIR differential absorption LIDAR systems
  - Standoff range: ~ 2x increase for fixed chem-bio sensitivity; scales as 1/√NEP
  - CB agent sensitivity: ~ 4x increase for fixed standoff range, scales as NEP
  - Compatible with 200 Hz line-tuned CO<sub>2</sub> laser

#### Technical Approach:

- Develop ultra-low noise receiver module (RM)
- Critical elements of receiver design required to achieve objectives:
  - Reduce baseline (background) photon flux on detector: Tunable Fabry-Perot etalon in optical train
  - Reduce input-referenced amplifier noise: custom amplifier
  - Reduce detector dark current: High impedance detector

#### Performance Metrics:

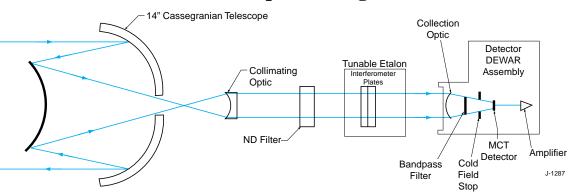
- Noise equivalent power of receiver system (NEP)
- Etalon tuning speed/bandwidth and wavelength positioning accuracy
- Electronics bandwidth

## **LIDAR Receiver Concept**

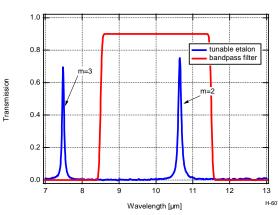


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#### **Conceptual Design**



#### **FP Etalon Transmission**



$$NEP_{total} = \left[ NEP_{Jsn+Amp+leak}^2 + NEP_{BLIP}^2 \right]^{1/2}$$

- Single element detector (HgCdTe) with band pass filter coupled to low noise custom amplifier → reduce NEP<sub>Jsn+Amp+Leak</sub>
- Insert tunable Fabry-Perot etalon in afocal region of optical train to reduce baseline flux on detector (~30x reduction) → reduce NEP<sub>BLIP</sub>
  - Etalon tracks 200 Hz CO<sub>2</sub> laser emission wavelength
  - Tunable etalon is PSI innovation
- f/0.9 optical system for full integration with the existing 14" Cassegranian telescope currently employed in the ECBC's FAL system

# Fabry-Perot Etalon: Overview



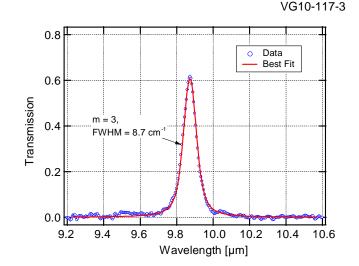
- Reduction of baseline flux on detector via tunable etalon insertion reduces system noise
  - Photon statistical noise: NEP ∞ (flux)<sup>0.5</sup> / (optics transmission)
- Transmission maxima fulfill Fabry-Perot resonance condition:

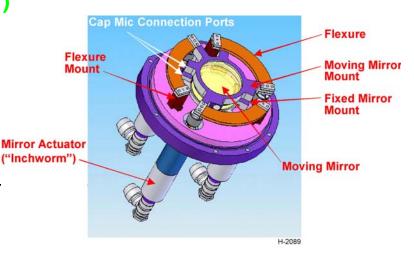
$$\lambda_m = \frac{2d}{m} \stackrel{\text{mirror spacing}}{\longleftarrow} \text{interference order (integer)}$$

Tuning range = Free Spectral Range:

$$\Delta \lambda \equiv \lambda_{\max,m} - \lambda_{m+1} (\lambda_{\max,m}) \approx \frac{\lambda_{\max,m}}{m+1}$$

- PSI etalon design:
  - Optics: 50 mm dia x 8 mm thick ZnSe, central 36 mm HRcoated
  - <u>Electronics:</u> FPGA-based control system increases the bandwidth of the etalon control loop and maintains active, continuous alignment of the etalon mirrors (control bandwidth between 2 kHz and 5 kHz)

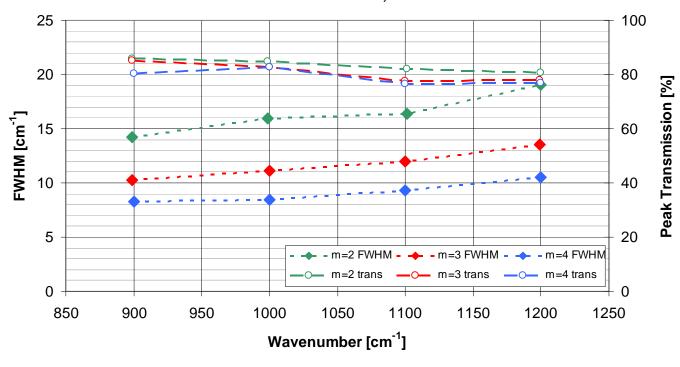




# Fabry-Perot Etalon: Spectral Performance Characteristics Physical Sciences Inc.

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#### 1559 Etalon Performance, December 09

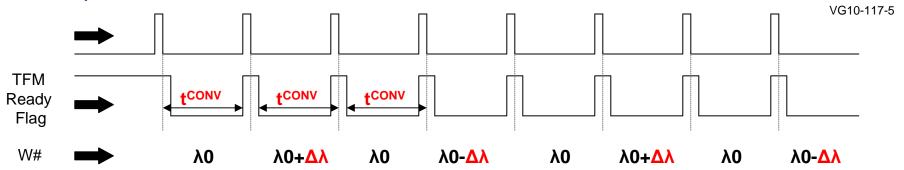


### Conclusions:

- Transmission ~ 80% for all orders across tuning range
- FWHM (m=2): 15 − 19 cm<sup>-1</sup>
- FWHM (m=3): 10 − 14 cm<sup>-1</sup>
- FWHM (m=4): 8 11 cm⁻¹

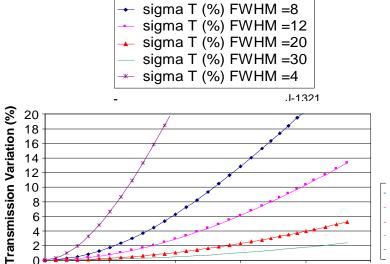
# Fabry-Perot Etalon: Derived Requirements





- Etalon transmission fringe needs to track CO<sub>2</sub> emission wavelength
  - 200 Hz laser → etalon needs to reach commanded wavelength in < 5 msec</li>
  - CO<sub>2</sub> laser lines:
    - Four branches: 9R, 9P, 10R, 10P
      - ~ 50% CO<sub>2</sub> lines require < 5 cm<sup>-1</sup> jumps
      - ~ 80% CO<sub>2</sub> lines require < 10 cm<sup>-1</sup> jumps
- Achieve < 1% transmission error due etalon wavelength position uncertainty
  - If the transmission varies from shot to shot, then the wavelength variation aliases as measurement noise and degrades CB agent detection sensitivity

$$\sigma_{
ho} \propto \sigma_{I/I_0} / (I/I_0) = \frac{\sigma_T}{T}$$



1.5

Variation In Fringe Position (cm-1)

2.5

0.5

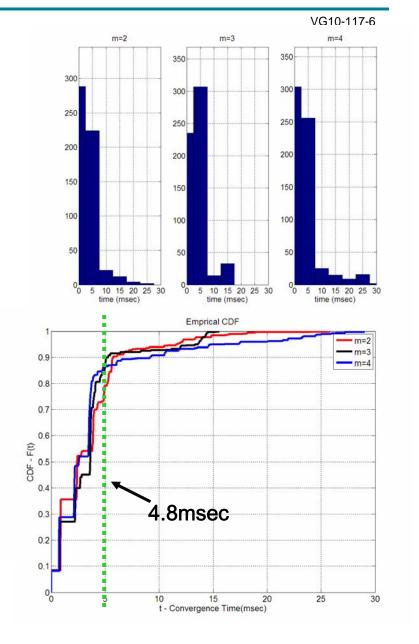


# Fabry-Perot Etalon: Tuning Speed

	m=2	m=3	m=4
5cm <sup>-1</sup> Jump	< 4ms	< 3.5ms	< 3ms
10cm <sup>-1</sup> Jump	< 5ms	< 4ms	< 4ms
40cm <sup>-1</sup> Jump	< 10ms	< 15ms	< 20ms
ECBC Wavelength List	< 5ms (80%)	< 5ms (85%)	< 5ms (85%)

### Etalon Tuning Performance:

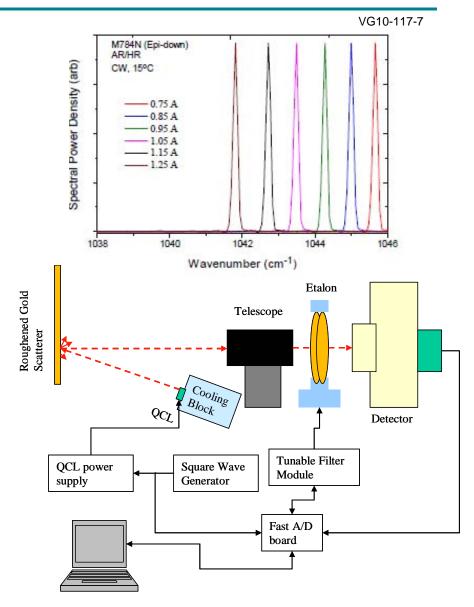
- Less than 5 ms convergence time for 10cm<sup>-1</sup> and smaller jumps
- Technical requirement successfully achieved
- Non-lasing laser trigger pulses are required for jumps greater than 10cm<sup>-1</sup>
  - Slightly reduced the system duty cycle



# **Fabry-Perot Etalon:**

# Transmission Uncertainty Measurements (1) Physical Sciences Inc.

- Make use of Quantum Cascade Laser (QCL, Maxion P/N M784) which emits at 9.6 μm
  - Direct measurement of the desired performance one can expect with the ECBC's FAL CO<sub>2</sub> laser
  - Multiple etalon scans over laser line
- Laser output was directed onto a roughened gold scattering screen
  - QCL was mounted to a cooling block and directed through a collimating lens onto the screen
  - A N<sub>2</sub>(I)-cooled LWIR camera was used to monitor the onset of lasing and to adjust the lens
- The laser power supply was modulated with a square wave to +/- 30mA at 10 kHz
  - Laser turned on and off in a binary fashion with a 50% duty cycle
  - Produced a detectable AC signal well above the detector's high pass cutoff frequency of 500 Hz

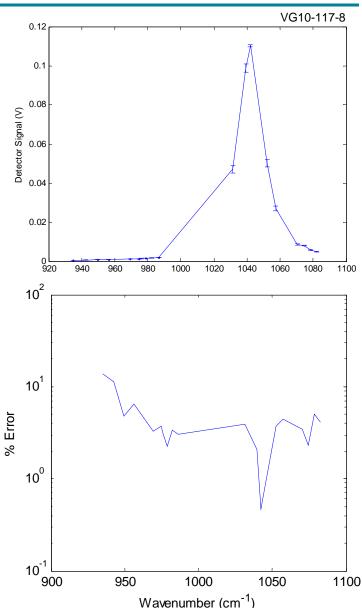


# Fabry-Perot Etalon: Transmission Uncertainty Measurements (2) Physical Sciences Inc.

- The QCL emission is significantly narrower than the etalon transmission bandwidth
  - Shape of the peak represents the etalon transmission function
- Each wavelength data point is an average of 32 separate measurements (etalon scans) and error bars are the standard deviation:

$$\%Error = (\frac{\sigma(stdev)}{Mean}) \cdot 100$$

- The transmission error due to etalon wavelength position uncertainty is ~ 0.5%
  - Successfully meet derived requirement
- The etalon convergence criteria is determined based on optimization of both tuning speed and position accuracy

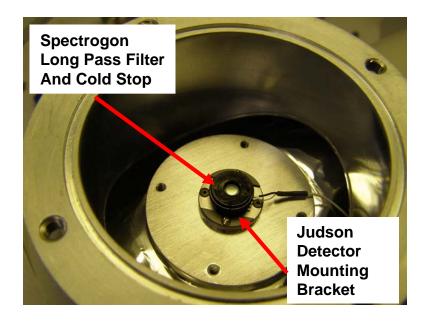


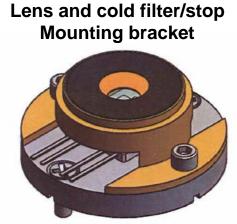
### **Detector**



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- Judson single element PVMCT, 0.5 mm diameter
  - Capacitance ~ 200 pF
  - 77K resistance @ 0 VDC: 11 kΩ
- The detector mounting bracket was custom designed to support the integration of the collection lens assembly inside the dewar for reduction of self-radiance of optical components





### **Custom Preamplifier**



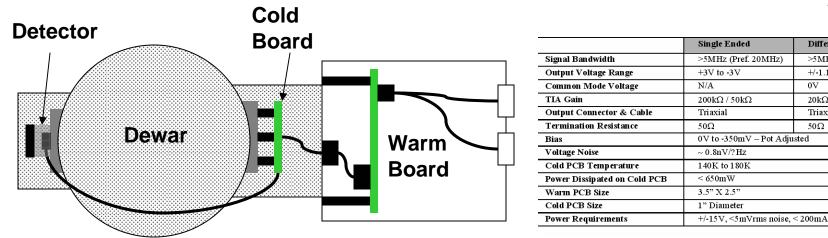
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Differential >5MHz (Pref. 20MHz)

+/-1.13V

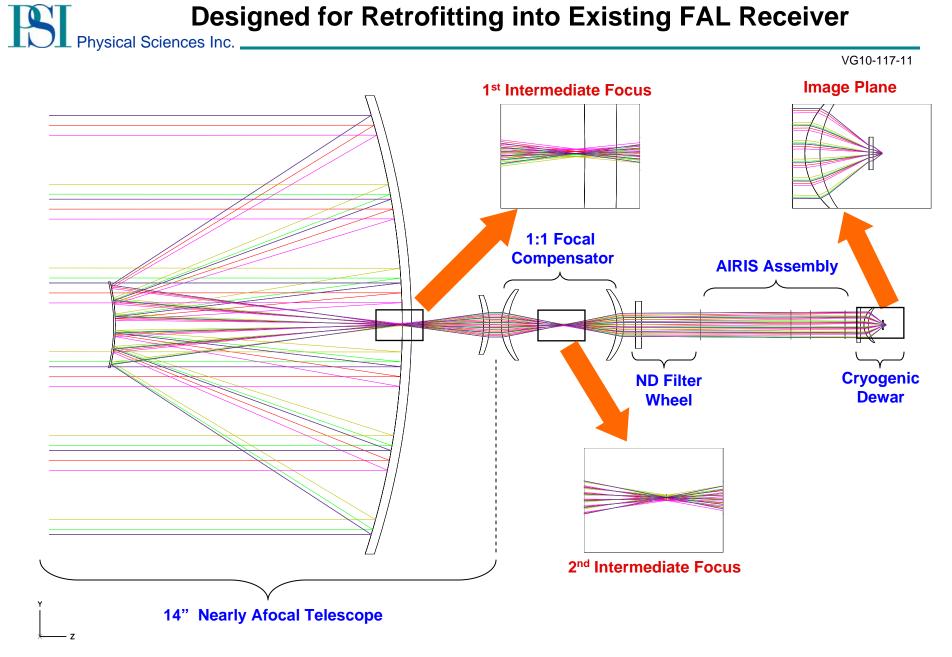
 $20k\Omega / 5k\Omega$ Triaxial (2X)

0V



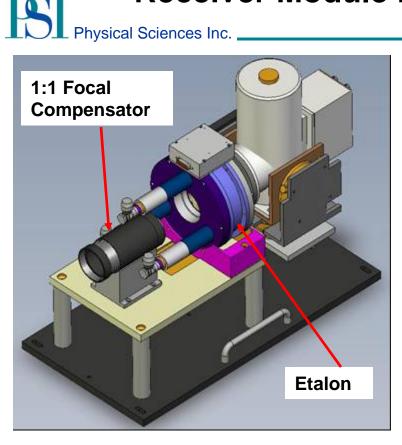
- The transimpedance preamplifier architecture was optimized around the selected IR detector diode
  - Input-referenced noise density of 0.8 nV/ Hz<sup>0.5</sup>
- A portion of the preamplifier was physically located within the cryogenic dewar with the IR photodiode
  - Stage consists of a JFET transistor with the detector attached to its gate
    - Thermal noise from this stage and any stray capacitance at the input are reduced
    - Reductions help to lower the input referred noise added by the preamplifier.
- The other portion of the preamplifier was located directly outside the dewar and was operated at room temperature
  - The majority of the preamplifier circuitry is located on this PCB
    - Circuitry to control and adjust bias condition
    - Monitor dewar temperatures
    - Buffer the preamplifier output

## **Optical Layout:** Designed for Retrofitting into Existing FAL Receiver

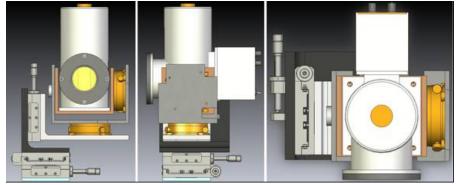


### Receiver Module Mechanical Configuration

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### **Detector Mounting Stage**





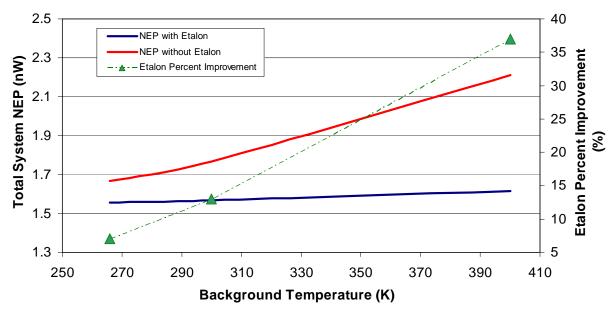
- Assembly designed for ease of integration into FAL system
- Detector mounted on a Yaw, Tilt, XYZ translation stage for easy optical alignment

# FAL Receiver Module: Performance Characterization, System Model

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- Model system performance
  - Model developed in Matlab
  - Model calculates NEP<sub>BLIP</sub> given specific system input parameters
- System NEP improvement most significant when observing warmer backgrounds which add significantly to the BLIP noise
  - ~37% improvement at T<sub>bkgd</sub>=400K
  - ~6% improvement at  $T_{bkad} = 266K$



 Experimentally determine system NEP for an electronic bandwidth of 5 MHz and compare with model predictions

# FAL Receiver Module: NEP Asymptote Measurement

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- Measure NEP contributed by detector thermal noise and preamp. noise (Johnson, voltage, current and leakage noise) – no BLIP noise
  - Replace cooled lens with blackened piece of aluminum
- Capture noise density using spectrum analyzer (PSD)

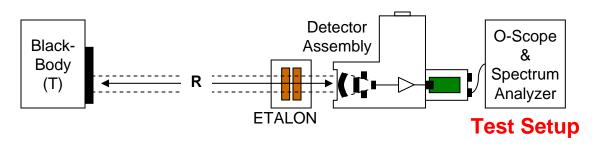
$$NEP_{total} = \left[ NEP_{Thermal+AmpV,I,Jsn+Leak}^{2} + NEP_{BLIP}^{2} \right]_{2}^{1/2}$$

$$NEP_{total} = \frac{1}{R} \left[ \int_{0}^{5MHz} PSD(f) df \right]_{2}^{1/2}$$

	Gain (Low)	Gain (High)	Bandwidth	NEP (@ 80K) 5 MHz, High Gain
Single Ended	52.98kΩ	213.1kΩ	~16MHz	1.54 nW
Differential	4.64kΩ	18.56kΩ	~20MHz	*

# FAL Receiver Module: NEP<sub>BLIP</sub> Measurement



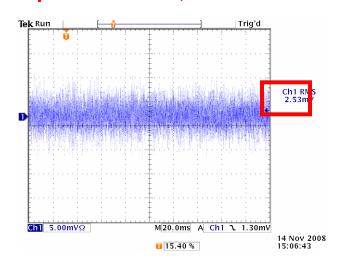


$$NEP_{BLIP}(nW) = \frac{\sqrt{(RMS_{Total})^2 - (RMS_{Gold\_Mirror})^2}}{D_{responsivity}(A/W) \cdot Gain(k\Omega) \cdot (10^6)}$$

- Measure noise baseline by observing gold mirror (looking at ~77K target) positioned in front of detector window
- Tune Etalon to a single wavelength and observe 400K Blackbody
- Measure total NEP using noise PSD captured by spectrum analyzer (or RMS noise on O-scope) with and without etalon inserted in the optical train
- Calculate NEP<sub>RLIP</sub> with and without etalon



#### O-scope RMS Noise, Etalon @ m=2



# **FAL Receiver Module:** Physical Sciences Inc. Performance Characterization Summary

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@5MHz, T <sub>bkgd</sub> =400K	m=2	m=3	m=4	No Etalon
NEP-Det/Preamp	1.54nW	1.54nW	1.54nW	1.54nW
NEP-Blip (Measured)	0.73nW	0.64nW	0.61nW	1.86nW
NEP-Blip (Modeled)	0.48 nW			1.59nW
Measured NEP <sub>total</sub>	1.70nW	1.67nW	1.66nW	2.42nW
Modeled NEP <sub>total</sub>	1.61nW			2.21nW

- Objective: NEP ≤ 1.5nW for 5 MHz bandwidth
- Overall NEP is ~13% higher than design goal
  - Higher detector capacitance than expected increased NEP
- Measured NEP improvement through the use of etalon consistent with expected performance
  - ~ 37% NEP improvement when  $T_{bkqd}$ =400K

## **RM Integration into FAL System**



VG10-117-17

- Receiver Module (RM) transported to ECBC for full system integration
  - Dec 16 18, 2009
- Successfully performed system optical alignment
  - Developed alignment procedure
  - Demonstrated the ability to remove RM in & out and retain the integrity of the optical alignment

# Successfully integrated RM/TFM with FAL software/hardware

- Confirmed TFM can be controlled by FAL software
  - Using DLL functions developed by PSI
- Characterized integrated TFM operation (with FAL laser on)
  - TFM Convergence time and sigma values
  - Burst and Laser Triggers with non-lasing triggers inserted
  - Etalon scanning and transmission measurements error against known FAL laser line/s





# RM/FAL System: Performance Characterization

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#### Performed system characterization

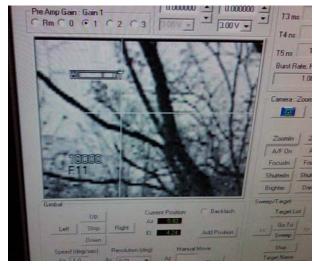
 Goal: Characterize FAL/RM system noise and overall improvement due to the use of the etalon

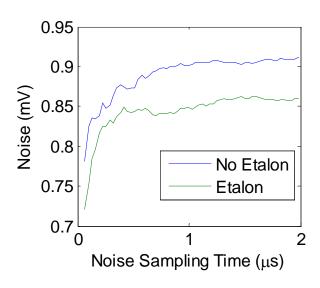
#### Targets:

- Hard target @ ~ 400 m (tree branch)
- $T_{bkad} \sim 266K$

#### System Measurements:

- Single laser shots (10R20) with etalon fixed at 975 cm<sup>-1</sup>
- Single laser shots (10R20) with etalon tuning across the laser line
- Laser scanning (9 lines) with etalon synched and scanning
- Blip noise measurements are made by analyzing the noise in the digitizer's traces in the absence of laser light
- Analyzed noise gives a good estimation of the Noise Equivalent Voltage, which can be converted to NEP
  - It is important that laser returns be negligible by t<sub>1</sub> so that the time dependent laser return signal does not contribute to the measured noise.
  - Results demonstrate a ~ 6% NEP improvement through the use of PSI's etalon in the FAL system
  - Results consistent with modeling predictions when system observing a T<sub>bkad</sub> ~ 270 K
- RM successfully demonstrated expected BLIP noise reduction





### **Conclusions**



VG10-117-19

- Successfully developed low noise receiver module for FAL
- Receiver module is fully compatible with 200 Hz line tuned
   CO<sub>2</sub> laser
- Receiver module achieves total system NEP ~ 1.7 nW for an electronic bandwidth of 5 MHz
- NEP<sub>Blip</sub> reduction consistent with modeling predictions
- Receiver module was successfully integrated with the ECBC's FAL system